

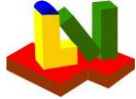
ASME BPVC VIII-1 2025
PTB-4-2021 / E4.3.7; E4.3.8

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Layout

Input values:	1.234	or	1.234
Calculated values:	1.234	or	1.234
Critical values:	1.234	or	1.234
Estimated values:	1.234	or	1.234

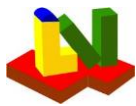


ASME BPVC VIII-1 2025
PTB-4-2021 / E4.3.7; E4.3.8

Summary

Strength Calculation Software	Program System ATLAS --- version : 11.0.8.24
Developed by Lauterbach Verfahrenstechnik GmbH	
Certified per DIN EN ISO 9001:2008	Certificate Number 01 100 044763

	LV Soft	ASME	Diff [%]
Example E4.3.7 - Conical transition Without a knuckle (large End)			
Required cylinder thickness t	37,48 mm 1,48 in	1,48 in	0,08%
Required cone thickness tr	39,93 mm 1,57 in	1,57 in	0,08%
Example E4.3.7 - Conical transition Without a knuckle (Small End)			
Required cylinder thickness t	23,78 mm 0,94 in	0,94 in	0,07%
Required cone thickness tr	25,25 mm 0,99 in	0,99 in	0,07%
Required area Ars	2.055,00 mm ² 3,19 in ²	3,19 in ²	0,03%
Required area Aes	5.081,53 mm ² 7,88 in ²	7,89 in ²	0,17%
Example E4.3.8 - Conical transition With a knuckle			
Required knuckle thickness t	17,20 mm 0,68 in	0,68 in	0,07%
Required cone thickness tr	24,74 mm 0,97 in	0,97 in	0,08%



E4.3.7 Large End - Cone-to-cylinder junction at large end under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2023

Cone-to-cylinder junction (wide end)

Type of reinforcing ring

(0 = no, 1 = at the cylinder, 2 = at the cone)

Without stiffener

Design pressure

Hydrostatic head

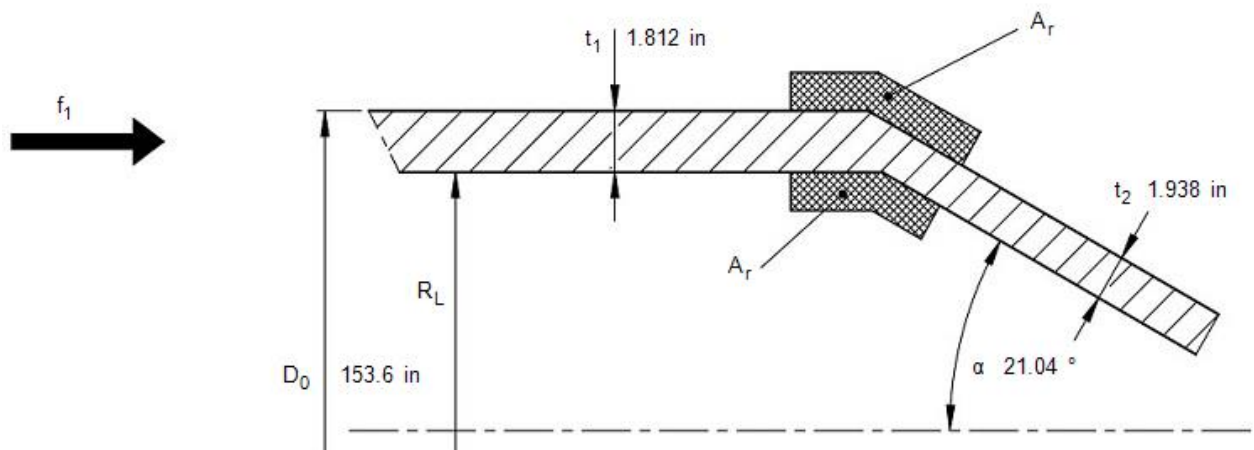
Calculation pressure

Calculation temperature

Axial load based on circumference (for compression negative)

p_D	356	psi
D_p	0	psi
p_0	356	psi
T_0	300	°F
f_1	0	lbf/in

0



Cylinder

Outside diameter

Final wall thickness

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

Allowance (corrosion)

Thickness without allowances

Inside radius

(= $D_0/2 - t_s$)

Allowable stress

Modulus of elasticity

Weld joint efficiency (or Cast Quality Factor)

D_0	153.6	in
t_1	1.812	in
c_1	0	in
c_2	0.125	in
t_s	1.687	in
R_L	75.12	in
S_s	20015	psi
E_s	2.829e+7	psi
E_1	1	

Cone

Half-apex angle ($\leq 30^\circ$)

Final wall thickness

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

Allowance (corrosion)

Effective thickness

Allowable stress

Modulus of elasticity

Weld joint efficiency (or Cast Quality Factor)

α	21.04	°
t_2	1.938	in
c_1	0	in
c_2	0.125	in
t_c	1.813	in
S_c	20015	psi
E_c	2.829e+7	psi
E_2	1	



Results

Geometrical conditions

valid

Strength condition

Wall thickness acceptable

Factor			k	1
Ratio		$P_0/S_s E_1$		0.01779
Angle	(Reinforcement required if $\Delta <$	21.04°	Δ	43.56 °
	α			
Effective load			Q_L	13371 lbf/in
Required thickness cylinder (UG-27)			t	1.351 in
with allowances (t_1)	1.812 in	$\geq t_+$	t_+	1.476 in
Required thickness cone (UG-32)			t_r	1.447 in
with allowances (t_2)	1.938 in	$\geq t_+$	t_+	1.572 in
Required cross sectional area			A_{rL}	0 in ²
Available cross section			A_{eL}	8.209 in ²
Required area of reinforcement			A_r	0 in ²
Available area of reinforcement		$b_v \cdot t_v$	A_v	0 in ²
Maximum distance from the connection point of the complete reinforcing area		$\sqrt{[R_L \cdot t_s]}$		11.26 in
centroid of reinforcing area		$0.25 \cdot \sqrt{[R_L \cdot t_s]}$		2.815 in

Equations

$$\cos(\alpha) = \cos(\alpha) \Leftrightarrow \cos(21.04^\circ) = 0.9333$$

$$\tan(\alpha) = \tan(\alpha) \Leftrightarrow \tan(21.04^\circ) = 0.3846$$

$$Q_L = P_0 \cdot \frac{R_L}{2} + f_1 = 2.455 \text{ MPa} \cdot \frac{1908 \text{ mm}}{2} + 0 \text{ N/mm} = 2342 \text{ N/mm}$$

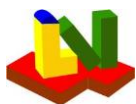
$$A_{rL} = \frac{k \cdot Q_L \cdot R_L}{S_s \cdot E_1} \cdot \left[1 - \frac{D_{el}}{\alpha} \right] \cdot \tan(\alpha) = \frac{1 \cdot 2342 \text{ N/mm} \cdot 1908 \text{ mm}}{138 \text{ MPa} \cdot 1} \cdot \left[1 - \frac{43.56^\circ}{21.04^\circ} \right] \cdot 0.3846 = 0 \text{ mm}^2$$

$$t = \frac{P_0 \cdot R_L}{S_s \cdot E_1 - 0.6 \cdot P_0} = \frac{2.455 \text{ MPa} \cdot 1908 \text{ mm}}{138 \text{ MPa} \cdot 1 - 0.6 \cdot 2.455 \text{ MPa}} = 34.3 \text{ mm}$$

$$t_r = \frac{P_0 \cdot \frac{R_L}{\cos(\alpha)}}{S_c \cdot E_2 - 0.6 \cdot P_0} = \frac{2.455 \text{ MPa} \cdot \frac{1908 \text{ mm}}{0.9333}}{138 \text{ MPa} \cdot 1 - 0.6 \cdot 2.455 \text{ MPa}} = 36.75 \text{ mm}$$

$$A_{eL} = (t_s - t) \cdot \sqrt{R_L \cdot t_s} + (t_c - t_r) \cdot \sqrt{R_L \cdot \frac{t_c}{\cos(\alpha)}} =$$

$$(42.86 \text{ mm} - 34.3 \text{ mm}) \cdot \sqrt{1908 \text{ mm} \cdot 42.86 \text{ mm}} + (46.04 \text{ mm} - 36.75 \text{ mm}) \cdot \sqrt{1908 \text{ mm} \cdot \frac{46.04 \text{ mm}}{0.9333}} = 5296 \text{ mm}^2$$



E4.3.7 Small End - Cone-to-cylinder junction at small end under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2023

Cone-to-cylinder junction (small end)

Type of reinforcing ring

(0 = no, 1 = at the cylinder, 2 = at the cone)

0

Without stiffener

Design pressure

p_D 356 psi

Hydrostatic head

D_p 0 psi

Calculation pressure

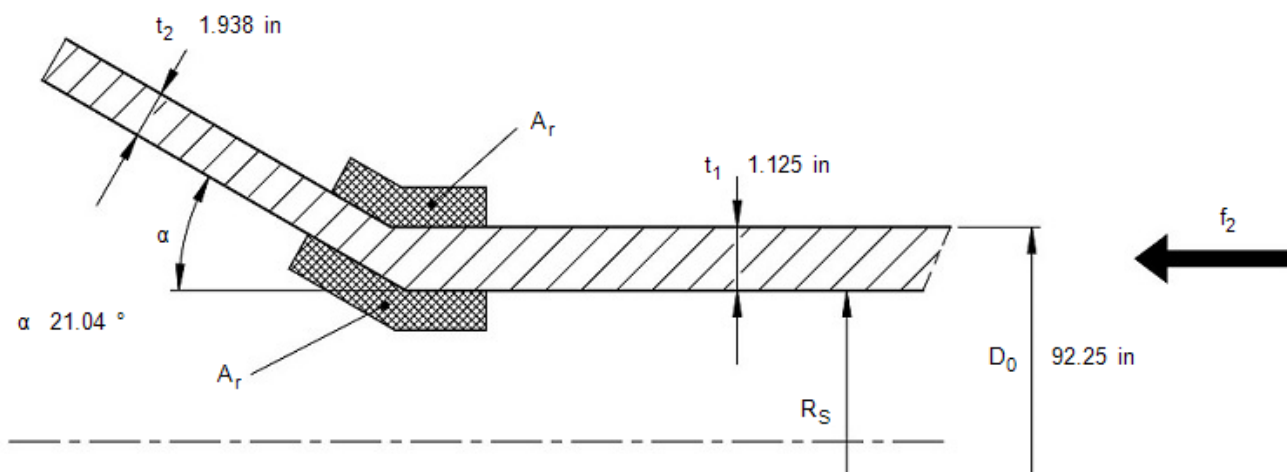
p_0 356 psi

Calculation temperature

T_0 300 °F

Axial load based on circumference (for compression negative)

f_2 396.9 lbf/in



Cylinder

Outside diameter

D_0 92.25 in

Final wall thickness

t_1 1.125 in

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

c_1 0 in

Allowance (corrosion)

c_2 0.125 in

Effective thickness

t_s 1 in

Inside radius

(= $D_0/2 - t_s$)

R_s 45.12 in

Allowable stress

S_s 20015 psi

Modulus of elasticity

E_s 2.829e+7 psi

Weld joint efficiency (or Cast Quality Factor)

E_1 1

Cone

Half-apex angle ($\leq 30^\circ$)

α 21.04 °

Final wall thickness

t_2 1.938 in

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

c_1 0 in

Allowance (corrosion)

c_2 0.125 in

Thickness without allowances

t_c 1.813 in

Allowable stress

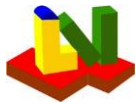
S_c 20015 psi

Modulus of elasticity

E_c 2.829e+7 psi

Weld joint efficiency (or Cast Quality Factor)

E_2 1



ASME BPVC VIII-1 2025

PTB-4-2021 / E4.3.7; E4.3.8

Results

Geometrical conditions

valid

Strength condition

Wall thickness acceptable

Factor			k	1
Ratio	$P_0/S_s E_1$			0.01779
Angle			Δ	11.87 °
Effective load			Q_S	8429 lbf/in
Required thickness cylinder (UG-27)			t	0.8113 in
with allowances (t_1)	1.125 in	$\geq t_+$	t_+	0.9363 in
Required thickness cone (UG-32)			t_r	0.8692 in
with allowances (t_2)	1.938 in	$\geq t_{r+}$	t_{r+}	0.9942 in
Required cross sectional area			A_{rS}	3.185 in ²
Available cross section			A_{eS}	7.876 in ²
Required area of reinforcement			A_r	0 in ²
Available area of reinforcement	$b_v \cdot t_v$		A_v	0 in ²
Maximum distance from the connection point of the complete reinforcing area	$\sqrt{[R_L \cdot t_s]}$			9.044 in
centroid of reinforcing area	$0.25 \cdot \sqrt{[R_L \cdot t_s]}$			2.261 in

Equations

$$\cos(\alpha) = \cos(\alpha) \Leftrightarrow \cos(21.04^\circ) = 0.9333$$

$$\tan(\alpha) = \tan(\alpha) \Leftrightarrow \tan(21.04^\circ) = 0.3846$$

$$QS = P_0 \cdot \frac{RS}{2} + f_2 = 2.455 \text{ MPa} \cdot \frac{1146 \text{ mm}}{2} + 69.5 \text{ N/mm} = 1476 \text{ N/mm}$$

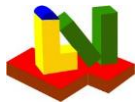
$$ArS = \frac{k \cdot QS \cdot RS}{SS \cdot E1} \cdot \left[1 - \frac{Del}{a} \right] \cdot \tan(\alpha) = \frac{1 \cdot 1476 \text{ N/mm} \cdot 1146 \text{ mm}}{138 \text{ MPa} \cdot 1} \cdot \left[1 - \frac{11.87^\circ}{21.04^\circ} \right] \cdot 0.3846 = 2055 \text{ mm}^2$$

$$t = \frac{P_0 \cdot RS}{Ss \cdot E1 - 0.6 \cdot P_0} = \frac{2.455 \text{ MPa} \cdot 1146 \text{ mm}}{138 \text{ MPa} \cdot 1 - 0.6 \cdot 2.455 \text{ MPa}} = 20.61 \text{ mm}$$

$$tr = \frac{P_0 \cdot \frac{RS}{(\cos(\alpha))}}{Sc \cdot E2 - 0.6 \cdot P_0} = \frac{2.455 \text{ MPa} \cdot \frac{1146 \text{ mm}}{0.9333}}{138 \text{ MPa} \cdot 1 - 0.6 \cdot 2.455 \text{ MPa}} = 22.08 \text{ mm}$$

$$AeS = 0.78 \cdot \sqrt{RS \cdot ts} \cdot \left[(ts - t) + \frac{(tc - tr)}{\cos(\alpha)} \right] =$$

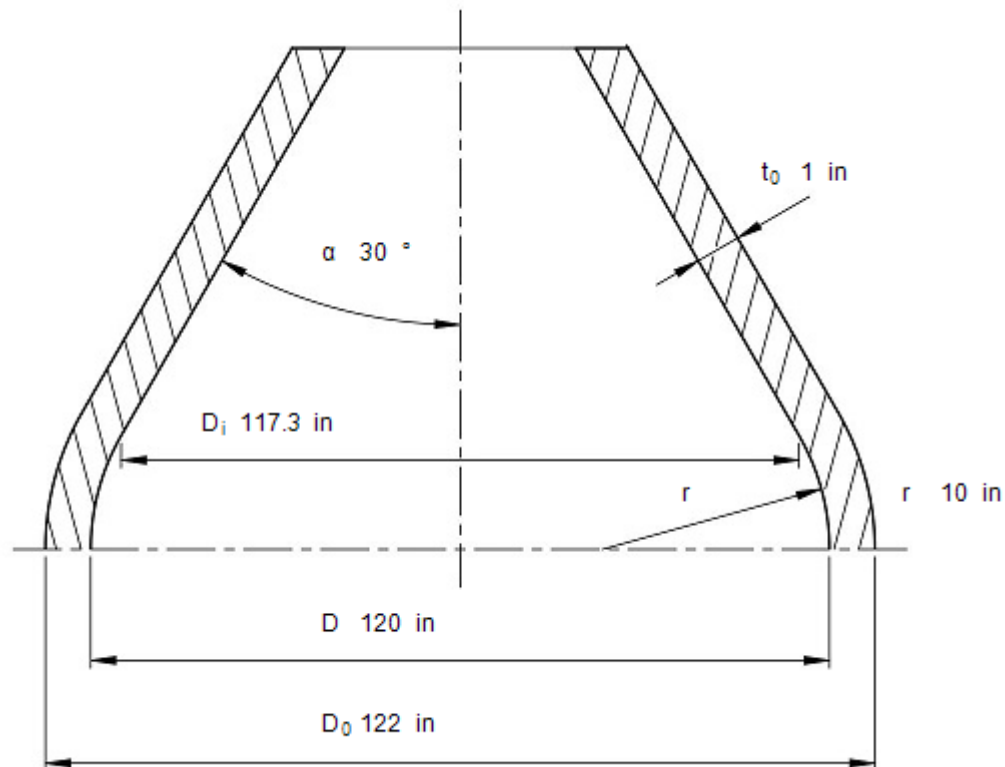
$$0.78 \cdot \sqrt{1146 \text{ mm} \cdot 25.4 \text{ mm}} \cdot \left[(25.4 \text{ mm} - 20.61 \text{ mm}) + \frac{(46.04 \text{ mm} - 22.08 \text{ mm})}{0.9333} \right] = 5082 \text{ mm}^2$$



E4.3.8 - Cone with knuckle under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2023

Toriconical sections

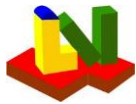
Design pressure	p_D	285.4 psi
Hydrostatic head	D_p	0 psi
Calculation pressure	p_0	285.4 psi
Calculation temperature	T_0	300 °F
Final wall thickness	t_e	1 in
Wall thickness allowance	c_1	0 in
Allowance (corrosion)	c_2	0 in
Effective thickness without allowances	t_0	1 in



Outside diameter of cylindrical shell	D_0	122 in
Inside diameter of cylindrical shell (= $D_0 - 2t_0$)	D	120 in
Semi-apex angle	α	30 °
Knuckle radius ($\geq 0.06 \cdot D_0$, $\geq 3 \cdot t_e$)	r	10 in
Weld joint efficiency (or Cast Quality Factor)	E	1

Material K02700-SA-516-70-Class:-Size:

Allowable stress S **20015** psi



ASME BPVC VIII-1 2025

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Calculation

Largest inside diameter of cone	D_i	117.3	in
Equivalent radius	L	67.74	in
Ratio	L/r	6.774	
Factor	M	1.401	
Required knuckle thickness	t	0.6773	in
Allowable inside pressure of knuckle	P	421	psi

Calculation diameter of cone	D_1	117.3	in
Required cone thickness at D_1	t_1	0.9741	in
Allowable inside pressure of cone	P_1	292.9	psi

Remark

Required thickness incl. allowances	$t+C_1+C_2$	$t+$	0.9741	in
Allowable excess pressure	$\text{Min}(P, P_1)$	P_m	292.9	psi
Allowable excess pressure without hydr. Head		MAWP	292.9	psi

Geometrical conditions

valid

Strength condition

Wall thickness acceptable

Equations knuckle

$$\cos(\alpha) = \cos(\alpha) \Leftrightarrow \cos(30^\circ) = 0.866$$

$$D_i = D - 2 \cdot r \cdot (1 - \cos(\alpha)) = 3048 \text{ mm} - 2 \cdot 254 \text{ mm} \cdot (1 - 0.866) = 2980 \text{ mm}$$

$$L = \frac{D_i}{2 \cdot \cos(\alpha)} = \frac{2980 \text{ mm}}{2 \cdot 0.866} = 1720 \text{ mm}$$

$$t = \frac{P_0 \cdot L \cdot M}{2 \cdot S \cdot E - 0.2 \cdot P_0} = \frac{1.968 \text{ MPa} \cdot 1720 \text{ mm} \cdot 1.401}{2 \cdot 138 \text{ MPa} \cdot 1 - 0.2 \cdot 1.968 \text{ MPa}} = 17.2 \text{ mm}$$

$$P = \frac{2 \cdot S \cdot E \cdot t_0}{L \cdot M + 0.2 \cdot t_0} = \frac{2 \cdot 138 \text{ MPa} \cdot 1 \cdot 25.4 \text{ mm}}{1720 \text{ mm} \cdot 1.401 + 0.2 \cdot 25.4 \text{ mm}} = 2.903 \text{ MPa}$$

Equations cone

$$t_1 = \frac{P_0 \cdot D_1}{2 \cdot \cos(\alpha) \cdot (S \cdot E - 0.6 \cdot P_0)} = \frac{1.968 \text{ MPa} \cdot 2980 \text{ mm}}{2 \cdot 0.866 \cdot (138 \text{ MPa} \cdot 1 - 0.6 \cdot 1.968 \text{ MPa})} = 24.74 \text{ mm}$$

$$P = \frac{2 \cdot S \cdot E \cdot t_0 \cdot \cos(\alpha)}{D_1 + 1.2 \cdot t_0 \cdot \cos(\alpha)} = \frac{2 \cdot 138 \text{ MPa} \cdot 1 \cdot 25.4 \text{ mm} \cdot 0.866}{2980 \text{ mm} + 1.2 \cdot 25.4 \text{ mm} \cdot 0.866} = 2.019 \text{ MPa}$$